by Fritz Ruoss

SR1/SR1+: Error from VDI 2230 regarding minimum screw-in depth corrected

Dr. Andreas Kroker discovered an error in the calculation of the minimum screw-in depth, which was also confirmed by the VDI. Thank you, SR1/SR1+ has been amended accordingly.

$$m_{\text{ges min}} = \frac{R_{\text{m max}} \cdot A_{\text{S}} \cdot P}{\left\{ C_1 \cdot C_2 \cdot \tau_{\text{BS min}} \left[\frac{P}{2} + (d_{2\min} - D_{1\max}) \tan 30^\circ \right] \cdot \pi \cdot d_{\min} \right\}} + 2 \cdot P$$
(213)

In equation (213) of VDI 2230:2015, "dmin" of the bolt should be replaced by "D1max" of the nut. D1max is smaller than dmin, resulting in a larger minimum screw-in depth and a lower stripping safety factor. This only applies to the "bolt thread critical" case. The printout now includes even more intermediate results for users who want to recalculate or understand the result.

Shear stress coefficient VDI2230	taub/Rm	0,620	
Strength ratio VDI2230	RS	1,349	
RS >= 1 -> bolt thread critical			
C1 coeff. VDI2230	C1	0,840	
C2 coeff. VDI2230	C2	1,037	
C3 coeff. VDI2230	С3	0,897	
Max/min m ges (bolt thread crit.)	meffbolt mm	13,2	9,0
Max/min m ges (nut thread crit.)	meffnut mm	11,2	7,7
Min.thread length engag. Rmmax VD	Imeffmin mm	13,2	
Min.thread length engag. Rmmin VD	Imeffmin- mm	9,0	
Min.thread length engag. FS VDI	 m min FS mm 	9,7	

Using application examples 1 to 5 from VDI 2230-1:2015, we recalculated how the changes affect the results. Stripping safety B1 to B5, numbers in parentheses before the change (with dmin instead of D1max).

B1: mtr/meffmin = 1.52 unchanged, because RS<1 (nut thread critical)

B2: mtr/meffmin = 0.82 (0.91), RS>1 (bolt thread critical)

B3: mtr/meffmin = 1.89 (2.00), RS>1 (bolt thread critical)

B4: mtr/meffmin = 0.95 (1.07), RS>1 (bolt thread critical)

B5: mtr/meffmin = 1.09 unchanged, because RS<1 (nut thread critical)

Changes only apply to the "bolt thread critical" case. In Examples 2 and 4, the thread strip safety factor is even less than 1. According to VDI 2230, the minimum screw-in depth does not need to be calculated because a standard nut is used. Correct, the nut is secure. However, the bolt thread may be stripped.

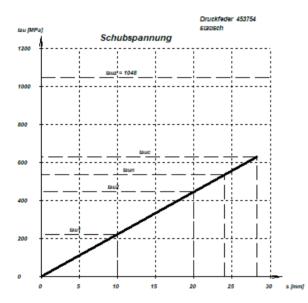
FED1+ 2+ 5 6 7 17: New calculation option: Always apply stress correction factor k

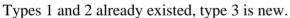
L tauz = 0.56 Rm for EN 10089 hot rolled	└── Warning: aW0 > d (safety spring)
🗹 tauk = tau * k (static+dynamic)	resolution 3D-Line 2 * <

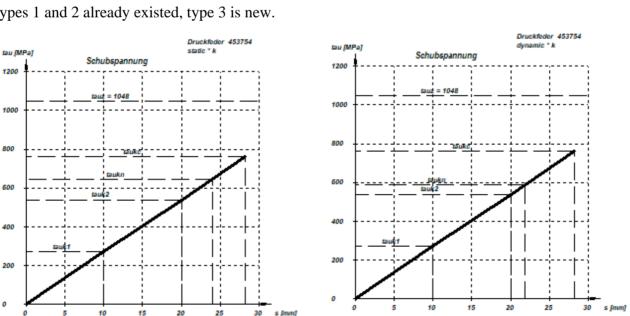
According to EN 13906, the stress correction factor k is only used for dynamically loaded springs, so corrected shear stresses (tau*k) tauk1, tauk2, taukh = tauk2 - tauk2 are only to be used for the working range. In British and American standards, however, the stress correction factor k is always used, even for purely statically loaded springs. Therefore, you can now check the box under "Edit/Calculation Method" to always include *k. This even has implications for dynamically loaded springs, because the block stress is then calculated using taukc instead of tauc.

There are now three different versions of the tau-s diagram (shear stress-spring deflection):

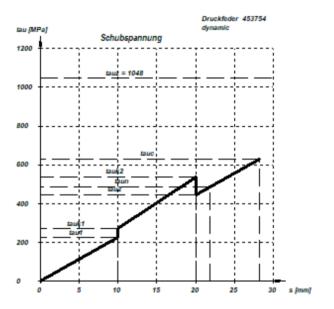
- 1: static without *k
- 2: dynamic without "*k static+dynamic"
- 3: *k static+dynamic







Type 3 is identical for static and dynamic application (only taukh differs).



FED1+ 2+ 5 6 7 17: Quick Views with/without "*k static+dynamic"

If "k static+dynamic" is set, the coefficients tau/tauz and tau/Rm are calculated with k in the Quick Views.

L [mm]	F [N]	tau [MPa]	s [mm]	tau/tau	z tau/Rn	n De	aW
L0: 60,00						25,00	3,59
L1: 50,00	F1: 131,9	tauk1: 269	s1: 10,00	0,26	0,14	25,04	2,32
L2: 40,00	F2: 263,7	tauk2: 539	s2: 20,00	0,51	0,29	25,07	1,05
Ln: 38,18	Fn: 287,7	taukn: 588	sn: 21,82	0,56	0,31	25,07	0,81
Lc: 31,77	Fc: 372,2	taukc: 760	sc: 28,23	0,73	0,41	25,08	0,00

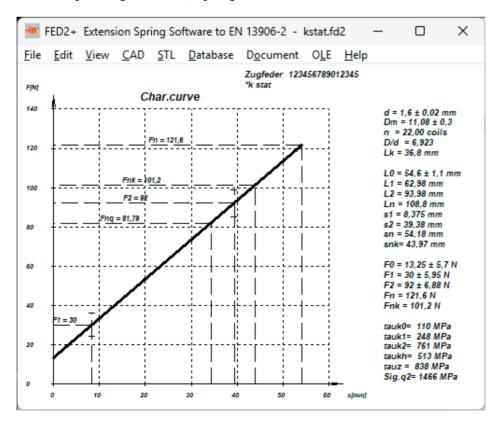
If "k static+dynamic" is not set, the coefficients tau/tauz and tau/Rm are calculated in the quick views as usual without k, including tau1 and tau2 for dynamic loading.

L [mm]	F [N]	tau [MPa]	s [mm]	tau/tauz	tau/Rn	n De	aW
L0: 60,00						25,00	3,59
L1: 50,00	F1: 131,9	tauk1: 269	s1: 10,00	0,21	0,12	25,04	2,32
L2: 40,00	F2: 263,7	tauk2: 539	s2: 20,00	0,43	0,24	25,07	1,05
Ln: 38,18	Fn: 287,7	tau n: 487	sn: 21,82	0,47	0,26	25,07	0,81
Lc: 31,77	Fc: 372,2	tau c: 630	sc: 28,23	0,60	0,34	25,08	0,00

Note tau/tauz and tau/Rm with *k (above) and without *k (below)

FED2+ with/without "k static+dynamic"

For FED2+, the "*k" setting uses tauk0, tauk1, tauk2, and taukn for calculations. For FED2+, taukn=tauz instead of taun=tauz, which reduces the usable spring length Ln in Lnk for tension springs at the corresponding (reduced) spring force Fnk.



FED2+: Loop names in production drawing



Form and Position of Loop loop 1: pic. A.6 (hook loop) loop 2: pic. A.6 (hook loop) loop rot. position: 0 ±28,2 deg

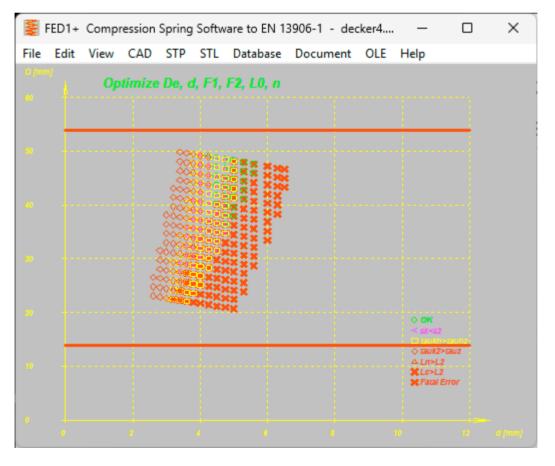
In the production drawing, only the EN number is used for the loops. You can now also configure the loop designation to be displayed in the production drawing.

However, you can also retain the previous display under "Edit\Production Drawing". International production drawings would always display the untranslated text, so the previous display is retained here.

loops Opic. A.6 (hook loo	p) / pic. A.6 (hook loop)		
O loops to EN 1390			
010000000000	72.2010 A. 07 0		

FED1+ Installation Space Design: Y-axis "D" instead of "De"

FED1+ calculates hundreds of springs for a given installation space, with warnings and error messages displayed as symbols in the diagram.



The labeling of the vertical axis with the coil diameter has been changed from "De" to "D." The upper limit is "De max," and the lower limit is "Di min." For the calculated springs, the wire diameter is marked "d" and the mean coil diameter is marked "Dm" (not "De").

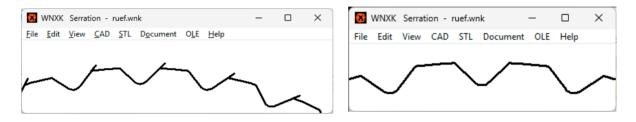
ZAR1,2,3,4,5,6,7,8,9: Gear material database

X5CrNi18-10 (1.4301) and AlZnMgCu1.5 were added to the gear materials database.

📉 Werkstoffdatenbank Rad	1			_	
<u>D</u> atei <u>A</u> nsicht <u>H</u> ilfe					
H A F	M	Suchen Weitersuchen	110 /110 (OK Abbrechen	
MAT_NAME	М	MAT_TYP	T	TREATMENT	HB_FLANK
X5CrNi18-10 (1.4301)	1	stainless steel	0	none	1
AlZnMgCul.5	8	Aluminium	0	none	1
—					

WNXK Profile Drawing

If the outer diameter of the splined shaft was smaller than the pitch diameter, an extra line was drawn in the shaft profile. The display has been corrected.



FED14: Layered coil springs



Such wave springs cannot be calculated with FED14. In FED14, the number of waves is 2.5, 3.5, 4.5; here it is 3.0, 4.0, 5.0. Such wave springs can only be calculated with FED13, or with FED14, one coil (n=1.0), then the spring force multiplied by the number of coils n. This is analogous to layered disc springs with FED4.

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